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- 1 -Anti-accretion additives for drilling fluids

This invention relates to anti-accretion additives for drilling
5 muds.

BACKGROUND OF THE INVENTION

Bit-balling and cuttings accretion are problems encountered when
10 drilling shales, particularly with water-based muds. Shale
cuttings can adhere to each other and to the bottom hole
assembly and cutting surfaces of the bit. Gradually a large
plastic mass builds up which can block mud circulation and
reduce rates of penetration. There is a "danger zone" of clay
15 plasticity for balling and accretion, related to the water
content of the clay or shale, which can be defined in terms of
the Atterberg limits of soil mechanics. In the dry zone the clay
has too little water to stick together and it is a friable and
brittle solid. In the wet zone the material is essentially
20 liquid like with very little inherent strength and can be washed
away.- Intermediate to these zones, i.e., in the danger zone,
the shale is a sticky plastic solid with greatly increased
agglomeration properties and inherent strength.

25 When cuttings are exposed to conventional water-based muds they
usually imbibe water and pass rapidly through these different
zones, eventually dispersing. However recent advances in
drilling fluid technology have developed highly inhibitive muds
which appear to reduce the hydration of shale and in doing so
30 maintain the cuttings in the danger or plastic zone contributing
to increased accretion and bit-balling. Field experiences with
glycol, phosphate and silicate muds in particular have shown
accretion problems.

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US patent 5,639,715 describes additives for bit-ballling prevention based on sulphonosuccinate chemistry.

Phosphorus based additives and compound have been used in the
5 oilfield industry mainly for the purpose of enhancing oil recovery from production wells.

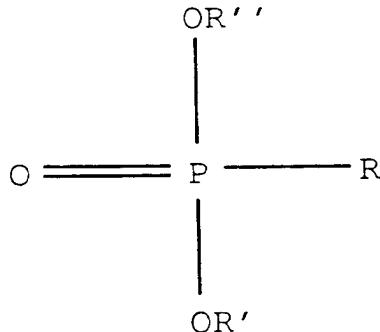
It is the object of the present invention to find alternatives to the known methods of preventing accretion.

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SUMMARY OF THE INVENTION

The invention is an additive for drilling mud. The additive
15 reduces the accretion and bit-ballling tendencies of cuttings exposed to said muds. The additives are based on phosphonate chemistry, and are preferably of the general class:

(I)



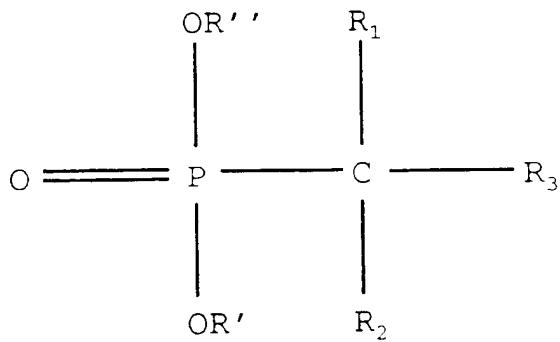
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wherein R, R' and R'' are radicals exclusively containing H atoms or combinations of H, C, O or P atoms up to a maximum of 100 atoms.

25 In a more preferred embodiment, the additives are based on the formula

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(II)



wherein R₁, R₂ and R₃ are radicals exclusively containing H atoms
 5 or combinations of H, C, O or P atoms up to a maximum of 100 atoms.

In a preferred embodiment of the invention, the additives are containing not more than one phosphor atom.

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In another preferred embodiment of the invention, the additive is a phosphor derivative of the succinic acid or short chain phosphorylated hydrocarbons.

15 Additives according to the invention are added to the drilling fluid at levels 0.1-10%, preferably 1-5%, weight by volume (%kg/liter). The drilling fluid itself may be oil based, though it is recognized that accretion tends to be less pronounced in drilling muds of this kind. Therefore, the preferred drilling
 20 fluid in accordance with the present invention is water based, even more preferably a reactive anionic based drilling fluid, such as silicate or phosphate based muds. Further additives as known in the art may be added to impart other desired properties to the mud system. Such known additives include viscosifying agents, filtrate reducing agents, and weight adjusting agents.
 25 Other preferred additives are shale-swelling inhibitors, such as salts glycol-, silicate- or phosphate-based agents, or any combination thereof.

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These and other features of the invention, preferred embodiments and variants thereof, and further advantages of the invention will become appreciated and understood by those skilled in the art from the detailed description below.

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MODE(S) FOR CARRYING OUT THE INVENTION

A test used to determine the anti-accretion properties of additives involves squeezing shale or clay cuttings between two 10 steel plates with a given force causing them to stick to each other and the plates. The force required to slide the plates apart is then determined using a force gauge or spring balance.

Oxford clay cuttings of size 2-4mm were soaked in the test fluid 15 for 15 minutes. The excess mud was drained from the cuttings using a sieve (500 micron mesh). A small pile of cuttings (5-10g) was put onto the base plate of the tester. The pile was roughly levelled and the top plate replaced over the cuttings. A PTFE spacer was placed on top of the top plate. A screw-mounted 20 plunger in the tester housing was wound down until it made contact with the spacer. A torque wrench was used to tighten the plunger onto the top plate. The standard torque was 75 inch-pounds (~9N.m). Immediately on reaching this value, the plunger was wound back sufficiently to remove the spacer. A force gauge 25 or spring balance was then connected to the top plate. The tension on the top plate was then increased by pulling on the force gauge until the plate breaks free from the cuttings bed. The maximum force recorded was the freeing force for the plate or accretion value. Values can range from 1.0 to above 20.0 kg 30 force.

The phosphonate based additives tested in accordance with the above procedure are added to a water-based mud containing tetrapotassium pyrophosphate (TKPP) and consisting of

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1000 ml fresh water (base)

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85.5 g tetrapotassium pyrophosphate (shale inhibitor)
2.85 g xanthan gum (viscosifier)
11.4 g carboxy methyl cellulose of low viscosity grade
(filtrate reducer)
5 42.75 g simulated drill solids
barite (weighting agent) to density 1.08 sg .
NaOH to pH 9.2
biocide

10 Baseline accretion values were established as:

Simple polymer mud	5 kg
TKPP mud	21.7 kg

15 The anti-accretion additives were then added to the TKPP mud at levels of 1-5%.

Additives which reduced the accretion value from >10 kg to 9 kg or below were:

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- Hydrolysed polymaleic acid
- 3-phosphonopropionic acid
- succinic acid
- propyl phosphonic acid

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- dibutyl-butyl phosphonate
- hydroxyphosphonoacetic acid
- dimethylpropyl phosphonate
- phosphorous acid
- diethyl-ethylphosphonate

30

- ethylmethacrylate phosphate
- tri-ethyl phosphonoacetate
- tetramethyl phosphonosuccinate
- phosphonosuccinic acid
- 2-hydroxyethyl phosphonic acid.

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The last five additives (Additives 9-14) were the found most effective. For those the following values were recorded:

TKPP mud + (%) additive: Accretion value

5	1% diethyl-ethylphosphonate	8 kg
	5% diethyl-ethylphosphonate	7 kg
	5% ethylmethacrylate phosphate	6 kg
	1% tri-ethyl phosphonoacetate	8 kg
10	5% tri-ethyl phosphonoacetate	5 kg
	5% tetramethyl phosphonosuccinate	7 kg
	5% phosphonosuccinic acid	7 kg
	5% 2-hydroxyethyl phosphonic acid.	7 kg

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In a second series of tests with the additives, silicate mud of the following composition was used:

1000 ml sea water (base)	
20 131 g Na silicate, a solution of 14% NaOH and 27% SiO ₂ (shale inhibitor)	
117.5 g KCl (shale inhibitor, weighting agent)	
20 g Polyanionic cellulose (filtrate reducer)	
5 g Xanthan gum (viscosifier)	
25 NaOH to adjust pH to 12.	

Baseline accretion values were established as:

simple polymer mud	9.5 kg
30 silicate mud	17.7 kg

The anti-accretion additives were tested in the silicate mud at 1% (w/v):

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Silicate mud + (1%) additive:Accretion value

	diethyl-ethylphosphonate	11.1 kg
	tri-ethyl phosphonoacetate	11.35 kg
5	tetramethyl phosphonosuccinate	9.96 kg
	phosphonosuccinic acid	10.8 kg
	2-hydroxyethyl phosphonic acid	11.4 kg

In most cases the accretion value has been reduced
10 significantly, down to the levels of a simple polymer mud.